

ZEROth LAW

Historically at this point people realized they needed to be more careful about temperature.

"If system A is in thermal equilibrium with B & C then B & C are in Ξ im with each other"

? ie no heat will flow between them

This law is needed if A is a thermometer & you want to believe B & C are at the same temperature.

EMPIRICAL TEMPERATURE

A classic measure of T is the length of a mercury column in a thermometer. Here one assumes

$$\theta(x) = ax + b$$

One fixes a & b with measurements

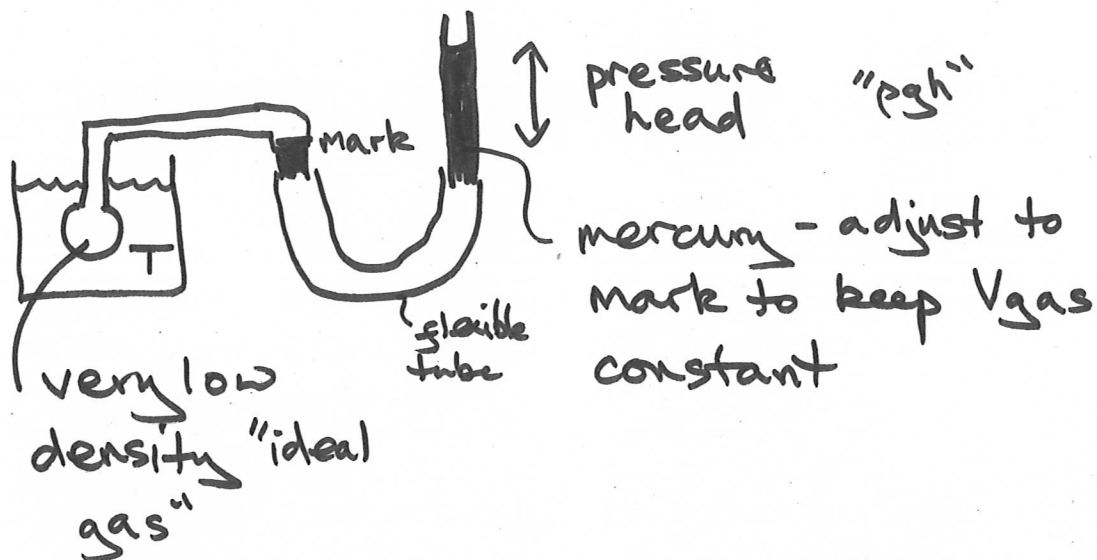
eg Centigrade $\theta = 0^\circ$ at water melting point

$\theta = 100^\circ$ at water boiling point

$$\Rightarrow \theta = 100 \left(\frac{x - x_0}{x_{100} - x_0} \right) \quad \begin{matrix} x = x_0 \rightarrow 0 \\ x = x_{100} \rightarrow 100 \end{matrix}$$

The precise melting & boiling points are hard to measure though... and there's a long extrapolation to -270°C .

Kelvin's Method



$$PV = n_m RT_I$$

At const V $T \propto P$

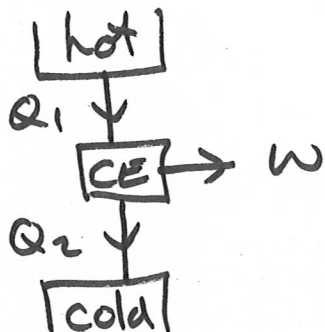
$$\Rightarrow T_I = 273.16 \left(\frac{P}{P_{TP}} \right)_{P \rightarrow 0}$$

At $T=0$ $P=0$ ✓

At triple point of water set $T=273.16$
→ this ensures a 100° difference between boiling & melting points.

Defining Temperature with Carnot Engines

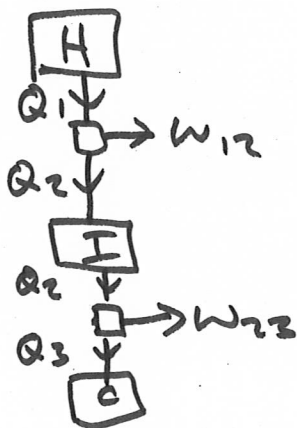
The most rigorous way to define temperature is using Carnot engines (the most efficient & reversible engine) - the idealized engine is independent of design.



The idea is to use Q extracted or dumped as a direct measure of temperature

$$Q = kT$$

A consistency check is



$$\frac{Q_1}{Q_2} = \frac{T_1}{T_2} \quad \& \quad \frac{Q_2}{Q_3} = \frac{T_2}{T_3}$$

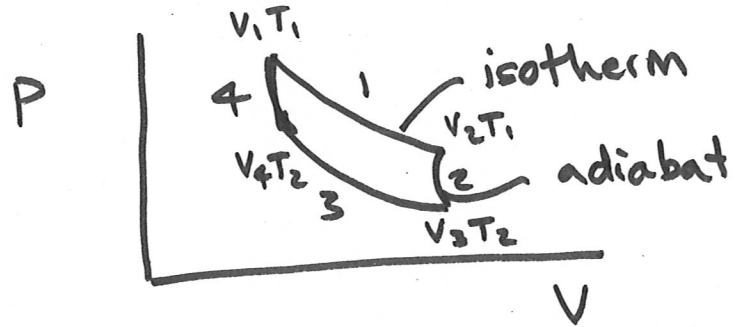
which means $\frac{Q_1}{Q_3} = \frac{T_1}{T_3} \checkmark$

Note $T=0$ gives no Q ... and then fix k with eg triple point of water $\rightarrow 273.16$ K again so the gap between boiling & freezing points is 100° .

$T_{CARNOT} = T_{IDEAL}$

Another good check of this T definition is that it directly works for ideal gas T_I

Carnot cycle:



- In step ① - isothermal expansion $T_I^{(1)} = \text{const}$

$$\begin{aligned}
 W_R &= - \int_{V_1}^{V_2} P dV \\
 &= - \int_{V_1}^{V_2} n_m R T_I^{(1)} \frac{dV}{V} \\
 &= n_m R T_I^{(1)} \ln V_1 / V_2
 \end{aligned}$$

The Q_1 lost by the hot sink is $Q_1 = n_m R T_I^{(1)} \ln \frac{V_2}{V_1}$

- In step ③ - isothermal compression at $T_I^{(2)} = \text{const}$

$$Q_2 = n_m R T_I^{(2)} \ln V_3 / V_4$$

So we would have

$$\frac{Q_1}{Q_2} \equiv \frac{T_1}{T_2} = \frac{T_I^{(1)}}{T_I^{(2)}} \frac{\ln V_2 / V_1}{\ln V_3 / V_4}$$

We can link the volumes by the adiabatic phases where $PV^\gamma = \text{const}$

$$\Rightarrow T_I V^{\gamma-1} = \text{const}$$

$$\textcircled{2} \quad T_I^{(1)} V_2^{\gamma-1} = T_I^{(2)} V_3^{\gamma-1}$$

$$\textcircled{4} \quad T_I^{(1)} V_1^{\gamma-1} = T_I^{(2)} V_4^{\gamma-1}$$

$$\div \quad \left(\frac{V_2}{V_1}\right)^{\gamma-1} = \left(\frac{V_3}{V_4}\right)^{\gamma-1}$$

$$\Rightarrow \frac{V_2}{V_1} = \frac{V_3}{V_4} \quad \& \text{ the logs above cancel.}$$

$$\text{ie} \quad \frac{Q_1}{Q_2} \equiv \frac{T_1}{T_2} = \frac{T_I^{(1)}}{T_I^{(2)}}$$

The ideal gas temperature & our empirical Carnot engine temperature are the same...
we can stop writing T_I !