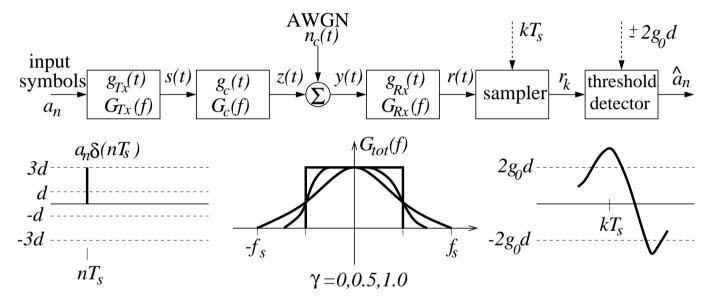
# **Revision of Modem so far**

- Previous three lectures have covered most of Modem, e.g.
  - Several digital modulation schemes, with emphasis on PSK and QAM
  - Mapping bits to symbols, type of constellations, and constellation design considerations
  - Carrier recovery (at least for BPSK, later we will generalise to QAM), this allows to remove carrier to get back to **baseband** signal
  - Time recover (at least for binary signalling, later we will generalise to multilevel signalling), this allows receiver **detector** to detect transmitted symbols and maps them back to bits
- This lecture, we exam baseband equivalent system and detector
  - Can any one answer what Tx & Rx filtering pair are designed for?
  - We will see the connection with **optimal detection**



### **Baseband Equivalent System**

- For M-QAM, I and Q branches are identical to one-dimensional  $\sqrt{M}$ -ary system
- **Baseband equivalent** I or Q system (with 16QAM example) is:



• Transmitted signal, received signal and sampled received signal are, respectively,

$$s(t) = \sum_{n} a_{n} g_{\text{Tx}}(t - nT_{s}), \quad r(t) = \sum_{n} a_{n} g_{\text{tot}}(t - nT_{s}) + n(t)$$
$$r_{k} = \sum_{n} a_{n} g_{n-k} + n_{k} = g_{0} a_{k} + \sum_{\substack{n \neq k}} a_{n} g_{n-k} + n_{k}$$



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### **Optimal Tx & Rx Filter Design**

- **Optimal design**: Tx & Rx filters are identical to square root of Nyquist raised cosine filter Note  $g_{tot}(t) = g_{Rx}(t) \star g_{c}(t) \star g_{Tx}(t)$  and  $\{g_n\}$  are symbol-spaced samples of  $g_{tot}(t)$
- 1. Achieve zero ISI:

$$\sum_{\substack{n \\ n \neq k}} a_n g_{n-k} = 0 \Longrightarrow G_{\text{tot}}(f) = G_{\text{Rx}}(f) G_c(f) G_{\text{Tx}}(f) \text{ is a Nyquist filter}$$

If  $G_c(f) = 1$ , the combined  $G_{Rx}(f)G_{Tx}(f)$  is a Nyquist filter

- 2. Maximise the received signal to noise ratio  $\Longrightarrow G_{Rx}(f) = G_{Tx}(f)$
- Linear system theory revisit

 $\frac{y(t)}{\Phi_{y}(f)}$ Recall power is the  $\begin{array}{c} g(t) \\ G(f) \end{array}$ x(t)Linear system  $\overline{\Phi_r(f)}$ area under PSD

PSD of system output y(t) is  $\Phi_y(f) = |G(f)|^2 \Phi_x(f)$ , and power of y(t) is thus

$$P_y = \int_{-\infty}^{\infty} \Phi_y(f) df = \int_{-\infty}^{\infty} |G(f)|^2 \Phi_x(f) df$$



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# Maximising SNR (continue)

• The channel noise has a PSD  $N(f) = \frac{N_0}{2}$  and it passes through  $G_{Rx}(f)$ , thus the noise power at receiver is:

$$P_N = \int_{-\infty}^{\infty} |G_{\rm Rx}(f)|^2 N(f) df = \frac{N_0}{2} \int_{-\infty}^{\infty} |G_{\rm Rx}(f)|^2 df$$

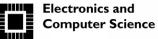
• Power of the transmitted signal s(t) is:

$$P_{\rm Tx} = \bar{a^2} \int_{-\infty}^{\infty} |G_{\rm Tx}(f)|^2 df = \bar{a^2} \int_{-\infty}^{\infty} \left| \frac{G_{\rm tot}(f)}{G_{\rm Rx}(f)} \right|^2 df$$

assuming  $G_c(f) = 1$ , where  $\bar{a^2}$  is the average symbol power

• Maximising the received SNR is equivalent to minimising  $P_N$  under the constraint of a constant  $P_{Tx}$ . Standard optimisation result yields:

$$G_{\mathrm{Tx}}(f) = G_{\mathrm{Rx}}(f)$$



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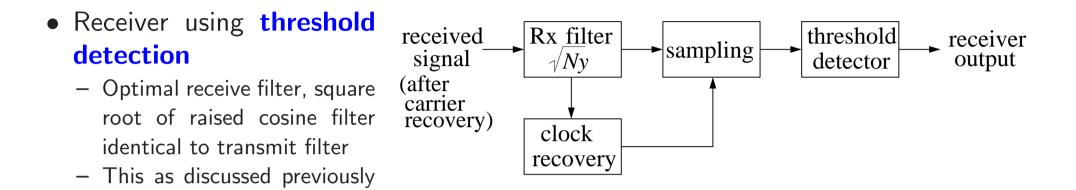
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### QAM Modem

- pulse • Re-plot transmitter of  $f_{\rm RF}$ shaping QAM Modem from Ι slide 77 *90*<sup>0</sup> S/P logical to  $\sqrt{Ny}$  $J_{\rm IF}$ convertor Gray cod. transmitted We have discussed all input bits signal 0 pulse operations in it shaping
- Now recall QAM receiver in slide 77
  - Received signal after carrier recovery is demodulated into I and Q baseband signals
  - Clock recovery is needed for each baseband signal to obtain timing information and a detector recovers the transmitted I & Q symbols
  - Finally, a de-mapping converts symbol stream into bit stream
- We will discuss carrier and clock recovery for QAM later
- Here we first concentrate on **detection** part
  - There are many equivalent detection schemes, and three common ones are discussed
  - They are equivalent, all based on principle of maximising received signal to noise ratio
  - Maximising received SNR, in ideal AWGN, is equivalent to minimise detection error



### **Threshold Detection**



• For 16QAM example, I and Q have a 4-ary constellation, and let symbols at levels 3d, d, -d and -3d be denoted as  $a_{+3}$ ,  $a_{+1}$ ,  $a_{-1}$  and  $a_{-3}$ 

The thresholds at detector are set to  $+2g_0d$ , 0 and  $-2g_0d$ , and the decision is made according to where the sample  $r_k$  lies:

$$\hat{a}_{k} = \begin{cases} a_{+3}, & \text{if } r_{k} > +2g_{0}d \\ a_{+1}, & \text{if } 0 < r_{k} \le +2g_{0}d \\ a_{-1}, & \text{if } -2g_{0}d < r_{k} \le 0 \\ a_{-3}, & \text{if } r_{k} \le -2g_{0}d \end{cases}$$

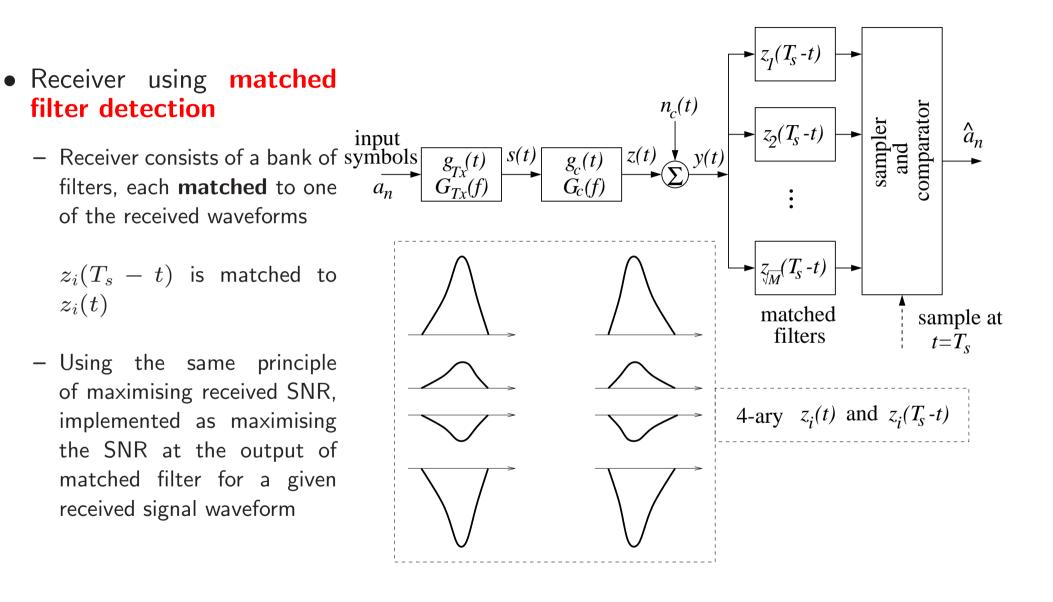


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maximises the SNR

### **Matched Filter Detection**



#### **Matched Filter Derivation**

• Input to the receive filter is:

$$y(t) = \sum_{n} a_{n}h(t - nT_{s}) + n_{c}(t) = z(t) + n_{c}(t)$$

where  $h(t) = g_{\mathrm{Tx}}(t) \star g_c(t)$ . Let matched filter output be  $r(t) = \bar{r}(t) + n(t)$ 

$$\bar{r}(t) = \mathcal{F}^{-1}[G_{\mathrm{Rx}}(f)Z(f)] = \int_{-\infty}^{\infty} G_{\mathrm{Rx}}(f)Z(f)e^{j2\pi ft}df$$

where  $Z(f) = \mathcal{F}[z(t)]$ . Note that  $r_k = \bar{r}_k + n_k$  and the noise  $n_k$  has a variance

$$\sigma_n^2 = \frac{N_0}{2} \int_{-\infty}^{\infty} |G_{\mathrm{Rx}}(f)|^2 df$$

• The aim is to maximise the SNR at sampling instant  $t = T_s$ :

$$\mathsf{SNR}_{T_s} = \frac{\bar{r}_k^2}{\sigma_n^2} = \frac{\left|\int_{-\infty}^{\infty} G_{\mathrm{Rx}}(f) Z(f) e^{j2\pi f T_s} df\right|^2}{\frac{N_0}{2} \int_{-\infty}^{\infty} |G_{\mathrm{Rx}}(f)|^2 df}$$



# Matched Filter Derivation (continue)

• Using Schwartz's inequality leads to

$$\left|\int_{-\infty}^{\infty} G_{\mathrm{Rx}}(f) Z(f) e^{j2\pi fT_s} df\right|^2 \leq \int_{-\infty}^{\infty} |G_{\mathrm{Rx}}(f)|^2 df \cdot \int_{-\infty}^{\infty} |Z(f)|^2 df$$

with equality holds if

$$G_{\rm Rx}(f) = cZ^*(f)e^{-j2\pi fT_s}$$

where  $\ensuremath{^*}$  denotes the complex conjugate

• With this optimal  $G_{\mathrm{Rx}}(f)$ ,  $\mathsf{SNR}_{T_s}$  is maximised

$$\mathsf{SNR}_{T_s}^{\max} = \frac{2}{N_0} \int_{-\infty}^{\infty} \left| Z(f) \right|^2 df$$

• The optimal receive filter in time domain is then given by

$$g_{\mathrm{Rx}}(t) = \mathcal{F}^{-1}[cZ^*(f)e^{-j2\pi fT_s}] = \begin{cases} c \cdot z(T_s - t), & 0 \le t \le T_s \\ 0, & \text{otherwise} \end{cases}$$



# **Matched Filter Summary**

Recall matched filter structure in slide 91

• The received z(t) takes waveforms  $z_i(t)$ ,  $1 \le i \le \sqrt{M}$ , each corresponding to a symbol point. If  $G_c(f) = 1$ ,  $z_i(t) = s_i(t)$ , waveforms of transmitted signal s(t)

As s(t) has a shape of square root of Nyquist raised cosine pulse, Rx filter  $g_{Rx}(t)$  has a similar shape. This is the same requirements of optimal Tx & Rx filtering

• The matched filter receiver consists of a bank of filters  $z_i(T_s - t)$ ,  $1 \le i \le \sqrt{M}$ , each of which is **matched** to one of the received waveforms  $z_i(t)$ ,  $1 \le i \le \sqrt{M}$ 

If the *j*th symbol point is transmitted, the waveform of z(t) is  $z_j(t)$ . The output of the matched filter  $z_j(T_s - t)$  will be the largest, and all the other matched filter outputs will be small

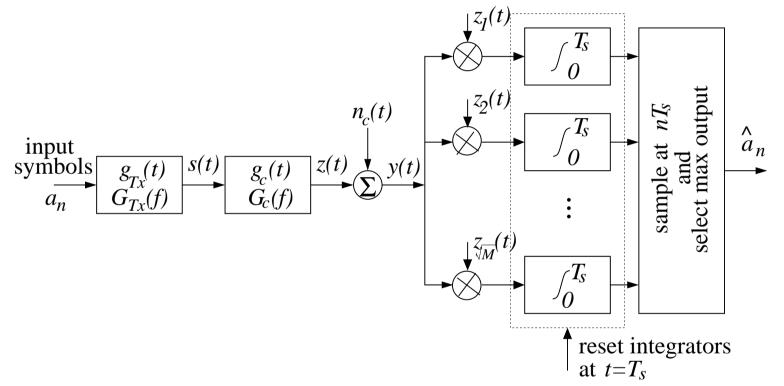
The comparator can easily infer which symbol point is transmitted

• Matched filter detector is a commonly used receiver structure. In practice,  $z_i(t)$  are unknown (channel is unknown), so  $s_i(T_s-t)$  are used



### **Correlation Receiver**

• Correlation receiver: an alternative implementation of matched filter receiver



• It first multiplies the received signal with the prototype signals  $z_i(t)$ ,  $1 \le i \le \sqrt{M}$ , integrates and dumps them at  $kT_s$ 

This is followed by a decision circuit to choose the largest output



# **Correlation Receiver Derivation**

• Integrator (receiver) output is convolution of received signal with receiver filter

$$r(t) = y(t) \star g_{\mathrm{Rx}}(t) = \int_0^t y(\tau) g_{\mathrm{Rx}}(t-\tau) d\tau$$

• Choosing c=1 in the optimal Rx filter  $g_{\rm Rx}(t-\tau)=c\cdot z(T_s-(t-\tau))$  leads to

$$r(t) = \int_0^t y(\tau) z(T_s - t + \tau) d\tau$$

• Integrate and dump at every  $t = T_s$ :

$$r(t=T_s)=r_k=\int_0^{T_s}y( au)z( au)d au$$

• In practice, received prototypes  $z_i(t)$ ,  $1 \le i \le \sqrt{M}$ , are unknown, and transmitted prototypes  $s_i(t)$  are used

# **Summary**

• Baseband equivalent system and optimal Tx & Rx filtering:

(1) achieve zero ISI, and (2) maximise the receive SNR, that is,

 $G_{\mathrm{Tx}}(f) = G_{\mathrm{Rx}}(f)$  and combined  $G_{\mathrm{Tx}}(f)G_{\mathrm{Rx}}(f)$  is a Nyquist filter

- QAM transmitter revisit
- QAM receivers: detector structure

Threshold detection receiver, matched filter receiver and correlation receiver

Their schematic diagrams, and how they works

They are equivalent and all based on the principle of maximising the receive SNR

Note that maximum Rx SNR is directly linked to minimum detection error



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